Modeling of the large deformation and the rupture of a metallic plate subjected to explosion

Benjamin Daudonnet, Frédéric Mercier, Krzysztof Woznica

To cite this version:

HAL Id: ineris-00976210
https://hal-ineris.archives-ouvertes.fr/ineris-00976210
Submitted on 9 Apr 2014
MODELING OF THE LARGE DEFORMATION AND RUPTURE OF A METALLIC PLATE SUBJECTED TO EXPLOSIVE LOADING

Benjamin Daudonnet / Baker Engineering and Risk Consultants, 304-5515 N. Service Road Burlington, Ontario, L7L 6G4 Canada

Frédéric Mercier / INERIS, Accidental Risk Department, BP 2, Verneuil en Halatte, 60550, France

Krzysztof Woznica / ENSI de Bourges, Institut PRISME, Laboratoire Energétique Explosion Structures EA 1205, 88, bd Lahitolle, 18020 Bourges Cedex – France

ABSTRACT
Thin walled metal pressure vessels or pipes commonly used in industry can burst under certain circumstances: as a result, the pressure envelope may undergo large deformations, which may eventually lead to a rupture. The response of these vessels to static and quasi-static loads is relatively well-understood but their response to highly dynamic pressure loading conditions is not.

This paper describes a numerical study of the response of circular metal plates to the dynamic loads produced by hydrogen-oxygen explosions. In this study, a range of dynamic responses and rupture criteria models are considered and compared with the results of experiments. The ability of MSC MARC software to model the rupture phase and, in some cases, the post-rupture phase (i.e., fragment production) is also discussed.

NOMENCLATURE
\( a = \) kinematic parameter, Pa
\( b = \) isotropic parameter
\( c = \) kinematic parameter
\( D = \) damage parameter
\( E = \) Young modulus, Pa
\( E = \) Young modulus modified by damage, Pa
\( J = \) scalar equivalent of deviatoric stress state, Pa
\( K = \) viscous parameter, Pa
\( k = \) initial yield limit
\( n = \) viscous parameter
\( \dot{p} = \) accumulated inelastic strain rate, s\(^{-1}\)
\( R = \) drag stress, Pa
\( R_i = \) isotropic parameter, Pa
\( s^\prime = \) deviator of stress tensor \( s \), Pa
\( T = \) temperature, K
\( X = \) back stress tensor, Pa
\( X' = \) deviator of back stress tensor \( X \), Pa
\( \alpha, \beta = \) parameters of damage law, Pa\(^{-1}\)
\( \varepsilon = \) strain
\( \varepsilon_r = \) limit of strain at rupture
\( \dot{\varepsilon} = \) inelastic strain rate, s\(^{-1}\)
\( \dot{\varepsilon}^\prime = \) inelastic strain rate tensor, s\(^{-1}\)
\( \gamma = \) parameter of Chaboche law, s\(^{-1}\)
\( \sigma = \) Von Mises equivalent stress, Pa
\( \sigma_{14} = \) hydrostatic stress, Pa
\( \sigma^* = \) stress triaxiality, Pa
\( P_i = \) pressure at ignition, bar

INTRODUCTION
A wide range of vessel rupture models models are available in the open literature. Some models, (i.e., Qiu et al. [17], Recho [18], Su et al. [21]) rely on the mechanical aspects of the failure such as crack propagation, while other models (i.e., Haque et al. [7], Leung [12], Woodward and Mudan [23], Fthenakis et al. [6]) treat the failure using fluid mechanics. Few models are available that consider both aspects of the failure. Where they exist, most studies in this behaviour are focussed on pipeline rupture, (i.e., Lung [8], Emery [4] and Rivalin [19], [20]).
In addition the modelling efforts listed, several experimental studies of structures subjected to a dynamic load have also been performed, for both simple ([5], [14], [15], [22], [16]) and complex structures ([11], [4]).

In this paper, experiments to measure the response of thin plates to various dynamic loads are presented. The experimental results illustrate the dynamic behavior and the rupture of the structure. These results were then compared to the results of a numerical model. The conclusions and the possible future use of the model are also presented.

**EXPERIMENTS**

**Experimental device**

The experimental device to test the metal plates, based on the one used in [24], is shown in Figure 1. Two stainless steel tubes were used: Tube 1 is 800 mm long and Tube 2 is 400 mm long. Each tube has an inside diameter of 194 mm and a wall thickness of 12.5 mm. The metal plate to be tested is clamped between these two tubes. Some experiments were performed with a rounded edge between the tube and the plate, in order to prevent the circumferential rupture caused by the sharp edge.

![Figure 1: Experimental Device](image)

Photo 1 displays the setup for the experiment. In addition to the elements already described above, a high speed camera (shown in the foreground) was used to record the crack propagation and pattern of the tested plates at 10000 frames/second. The experiments were conducted as follows. Once the testing plate was clamped between the tubes, a vacuum was simultaneously created in Tubes 1 and 2. A stoichiometric hydrogen-oxygen mixture was then introduced in Tube 1, while air was fed into Tube 2, to balance the pressure across the plate. Two kinds of explosion could then be produced:

- a "deflagration", in which the mixture was ignited by a low energy discharge (mJ range), such as an electric spark, or
- a "detonation", in which the mixture was ignited by a stronger ignition energy (50 J in our experiment). In this case, the shock wave is supersonic and very stable, resulting in a very repeatable dynamic loading condition, whereas deflagration case produced a more stochastic load.

When the shock wave reaches the tested plate, its velocity and overpressure peak are not those of a real detonation. For the purposes of discussion, the term "deflagration" also is used to refer to an explosion produced using the low energy ignition systems and the term "detonation" is used to describe the high ignition energy event, even though these terms are not exact for describing the two explosion modes.

A sample pressure trace from a detonation test is provided in Figure 2. The successive peaks represent the reflections of the wave inside the tube.

![Figure 2: Pressure-Time History - Detonation-(Pi=1.2 bar)](image)

**Experimental results**

Different plate thicknesses (2 mm, 1 mm and 0.5 mm) and materials (Al5754, Al2017, DC01) were tested. With the sharp edge, the plates were either bulged or split along the edge. With the rounded edge, the plates were also bulged but larger deformations were observed (Photo 2), as higher loadings could be applied without resulting in a circumferential rupture. For the Al5754 (1 mm) plates with the rounded edge, caps of different size (Table 1) were ejected (Photo 3): the rupture was not a shear rupture, as observed with the sharp edge.
Another way to initiate the rupture and control its starting location was to create a notch. Notches of different widths, from 0.3 mm to 1.6 mm, were created in the center of the plate. Photo 4 is an example of the results obtained for a 1 mm Al5754 notched plate.

Table 1: Diameter of Caps for Different Loads

<table>
<thead>
<tr>
<th>Initial pressure [bar]</th>
<th>1.1</th>
<th>1.2</th>
<th>1.4</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cap diameter [mm]</td>
<td>0</td>
<td>37</td>
<td>150</td>
</tr>
</tbody>
</table>

The elastoviscoplastic law of Chaboche [11] was chosen to describe the material behavior. It was demonstrated that this law gives accurate results, comparable to those obtained in experiments [24]. The relations introduced in this law are, for the inelastic strain rate \( \dot{\varepsilon}^i \):

\[
\dot{\varepsilon}^i = \frac{3}{2} \text{p} \frac{s'-X'}{J(s'-X')} \tag{1}
\]

where \( \text{p} \) is the accumulated inelastic strain rate,

\[
\dot{\text{p}} = \gamma \left( \frac{J(s'-X') - R - k}{K} \right)^n \tag{2}
\]

\( K \) and \( n \) are viscous parameters, \( \gamma = 1 \text{ [s}^{-1}] \). The parameter \( k \) is the initial yield limit.

\( s' \) denotes the deviator of stress tensor \( s \), \( \tilde{J} (...) \) is the scalar equivalent of deviatoric stress invariant. \( R \) is a drag stress. This law introduces an isotropic hardening:

\[
\tilde{R} = b(R_1 - R)^\delta \tag{3}
\]

where \( R_1 \) and \( b \) are material parameters.

A kinematic hardening is expressed through the evolution of the back stress \( \tilde{X} \),

\[
\dot{\tilde{X}} = 2a \tilde{\varepsilon}^i - cX \text{p} \tag{4}
\]

where \( a \) and \( c \) are the law parameters.

The following material data, validated for Al 5457 at \( T = 20^\circ \text{C} \) (Woznica et al., [24]), were used in the Chaboche viscoplastic model:

\[
\begin{align*}
E &= 71.11 \text{ GPa}, & \gamma &= 1 \text{ s}^{-1}, \\
n &= 8.9; & K &= 13.97 \text{ MPa}, \\
k &= 101.64 \text{ MPa}, & c &= 2478.3, \\
a &= 54049 \text{ GPa}, & b &= 14.68, \\
R_1 &= 178.45 \text{ MPa}.
\end{align*}
\]

Rupture criteria

The damage model proposed by Chaboche and Lemaitre [11] is a fully coupled model. It is based on the damage parameter \( D \) which can be expressed as a ratio between the Young’s Modulus modified by the damage and its initial value.

\[
D = 1 - \frac{E}{\tilde{E}} \tag{5}
\]

The value \( D = 0 \) corresponds to a non-damaged state, while \( D = 1 \) corresponds to a fully damaged (i.e., failed) state.

\[
\dot{D} = \left[ \frac{\sigma^2}{2E\alpha(l - D)} \right]^\beta \dot{\varepsilon}^i \tag{6}
\]

where \( \dot{f} \) is a function of the stress triaxiality.

The parameters \( \alpha \) and \( \beta \) corresponding to this damage law are expressed in equation (6). They can be using tensile loading/unloading tests where, \( f \) is a constant, [3].
While Chaboche was used as the basis for this study, other rupture criteria could also be used. To evaluate some of these alternatives, the following rupture criteria were also considered and defined into MSC Software:

- strain limit
  a simple strain limit obtained from tensile tests was used to define the rupture.
- strain rate:
  Another limit, based on the strain rate was also defined [9]:

  \[ \varepsilon_f = \left[ D_1 + D_2 \exp(D_3 \sigma^*) \right] \times \left[ I + D_4 \ln(\ddot{\varepsilon}) \right] \times \left[ I + D_5 T \right] \]

  where \( \varepsilon_f \) is the strain at rupture, \( \sigma^* \) is the triaxiality and \( \ddot{\varepsilon} \) is the non-dimensional strain rate,

- triaxiality damage:
  this criteria was used by Lee and Wierzbicky [10] for rupture of a thin plate under projectile loading as follows:

  \[ D_e = \int_0^{\varepsilon_f} \frac{\sigma_H}{\sigma} \, d\varepsilon \]

  where \( \sigma_H \) is the hydrostatic stress, and \( \sigma \) the Von Mises equivalent stress.

RESULTS
The numerical modeling and analysis were compared to the experimental results for both the ruptured and unruptured plate conditions.

Tests with no rupture
The MSC software model was validated by comparing the results obtained with those of Woznica et al. [24]. The close agreement between these results (2) indicates that the model is appropriate.

Additional comparisons to the experiments were then made:
- the final plate deflection along the radius was measured and compared to the numerically-predicted value at different times. As shown in Figure 3, good agreement between the numerical and the experimental results was observed.

Test 3: Plate Deflection at Different Times
(Deflagration, \( P_i = 0.8 \) bar, Sharp Edge)

- the large displacement and deformation of the plate observed when introducing a rounded edge plate holder also showed good agreement with the numerical results (Figure 4).

Figure 4: Numerical Displacement and Final Experimental Deflection at the Center of a Plate
(Detonation, \( P_i = 1.1 \) bar, Rounded Edge)

Following the verification of the deformation model using the Chaboche law, modeling of the rupture case was then studied.

Tests with rupture
Three different rupture tests were studied: un-notched plate with the rounded edge, notched tensile test specimen, notched explosive test specimen.

Un-notched Plate under Explosive Load
The rupture that occurs at high loadings with the rounded edge was studied using axisymmetric shell elements. Comparing the results obtained using different rupture criteria (i.e. strain, strain rate, damage) we notice that the best results (see Table 2) were obtained for criteria that take into account the strain rate or the damage (i.e., Chaboche-Lemaitre).
Table 2: Cap Radius Predictions

<table>
<thead>
<tr>
<th></th>
<th>Cap radius (mm)</th>
<th>Detonation $P_i = 1.2$ bar</th>
<th>Detonation $P_i = 1.4$ bar</th>
</tr>
</thead>
<tbody>
<tr>
<td>Experimental Result</td>
<td>Strain</td>
<td>18.5</td>
<td>75</td>
</tr>
<tr>
<td></td>
<td>Strain Rate ($\dot{\varepsilon}$)</td>
<td>39</td>
<td>59.52</td>
</tr>
<tr>
<td></td>
<td>Triaxiality Damage</td>
<td>24</td>
<td>56</td>
</tr>
<tr>
<td></td>
<td>Chaboche Lemaitre Damage Model</td>
<td>52.5</td>
<td>62.6</td>
</tr>
<tr>
<td>Predicted Cap Radius</td>
<td>30</td>
<td>72</td>
<td></td>
</tr>
</tbody>
</table>

These results illustrate the importance of the strain rate and the damage effect on the material response.

**Notched Tensile Test Specimen**

Before the studying of the failure of the notched plates under explosive loading, tensile test specimens were modelled. The aim of this experiment was to verify the adequacy of a method to model the rupture. We applied the strain criteria combined with the deletion of elements, as illustrated in Figure 5.

For Al2017, the crack length and velocity measured were compared to the calculated results. As presented in Figure 6 and Figure 7, good agreements were obtained, relative to the complexity of the phenomenon. This method could be applied for more elaborate arrangement, but any such model must be applied carefully as it can be subject to variation (for example if the size of the element is too large).
RECOMMENDATIONS FOR FUTURE WORK

While this study has shown good agreement for thin plates in a fixed geometry, a more detailed analysis of the limits of validity of this method is recommended. Another extension of this work would be to further study the projection of a fragment and its initial velocity once the rupture occurs. Indeed, in the case of the axisymmetric elements, the deletion of the failed element would lead to the creation of a fragment, which is then projected.

REFERENCES


